

Problem 1) $n_a(\omega) = \sqrt{\mu_a(\omega)\varepsilon_a(\omega)} = \sqrt{\varepsilon_a(\omega)}$. Similarly, $n_b(\omega) = \sqrt{\mu_b(\omega)\varepsilon_b(\omega)} = \sqrt{\varepsilon_b(\omega)}$.

a) $\mathbf{k}^{(i)} = k_x \hat{\mathbf{x}} + k_y \hat{\mathbf{y}} + k_z^{(i)} \hat{\mathbf{z}} = n_a(\omega)(\omega/c)(\sin \theta \hat{\mathbf{x}} - \cos \theta \hat{\mathbf{z}})$.

$\mathbf{k}^{(r)} = k_x \hat{\mathbf{x}} + k_y \hat{\mathbf{y}} + k_z^{(r)} \hat{\mathbf{z}} = n_a(\omega)(\omega/c)(\sin \theta \hat{\mathbf{x}} + \cos \theta \hat{\mathbf{z}})$.

$\mathbf{k}^{(t)} = k_x \hat{\mathbf{x}} + k_y \hat{\mathbf{y}} + k_z^{(t)} \hat{\mathbf{z}} = n_a(\omega)(\omega/c) \sin \theta \hat{\mathbf{x}} + k_z^{(t)} \hat{\mathbf{z}}$.

The dispersion relation $k_x^2 + k_z^2 = (\omega/c)^2 n_a^2(\omega)$ is used here. Also invoked is the generalized Snell's law.

b) Dispersion relation: $\mathbf{k} \cdot \mathbf{k} = k^2 = (\omega/c)^2 \mu_b(\omega)\varepsilon_b(\omega) \rightarrow k_x^2 + k_z^2 = (\omega/c)^2 n_b^2(\omega)$

$\rightarrow k_z^{(t)} = \pm \sqrt{(\omega/c)^2 n_b^2(\omega) - k_x^2} \rightarrow k_z^{(t)} = -i(\omega/c) \sqrt{n_a^2(\omega) \sin^2 \theta - n_b^2(\omega)}$.

Since $\theta > \theta_c$, we have $n_a \sin \theta > n_a \sin \theta_c = n_b$. Therefore, $k_z^{(t)}$ is negative, which makes its square root imaginary. We have chosen the negative sign for $k_z^{(t)}$ to ensure the exponential decay (as opposed to growth) of the evanescent field away from the interface (i.e., as $z \rightarrow -\infty$). This is now guaranteed, since the z -dependent factor in the expression of the fields, namely,

$$\exp(ik_z^{(t)} z) = \exp[(\omega/c) \sqrt{n_a^2(\omega) \sin^2 \theta - n_b^2(\omega)} z],$$

approaches zero when $z \rightarrow -\infty$.

c) $\mathbf{B}^{(t)}(\mathbf{r}, t) = \mu_0 \mu(\omega) H_{0y} \hat{\mathbf{y}} \exp[i(\mathbf{k}^{(t)} \cdot \mathbf{r} - \omega t)]$.

For $\nabla \cdot \mathbf{B}^{(t)} = i\mathbf{k}^{(t)} \cdot \mu_0 \mu(\omega) H_{0y} \hat{\mathbf{y}} \exp[i(\mathbf{k}^{(t)} \cdot \mathbf{r} - \omega t)]$ to vanish it is necessary to have

$\mathbf{k}^{(t)} \cdot \hat{\mathbf{y}} = (k_x \hat{\mathbf{x}} + k_z^{(t)} \hat{\mathbf{z}}) \cdot \hat{\mathbf{y}} = 0$, which obviously holds, since $\mathbf{k}^{(t)}$ has no y -component.

d) $\nabla \times \mathbf{H} = \partial_t \mathbf{D} \rightarrow i\mathbf{k}^{(t)} \times \mathbf{H}_0^{(t)} = -i\omega \varepsilon_0 \varepsilon_b(\omega) \mathbf{E}_0^{(t)}$

$\rightarrow (k_x \hat{\mathbf{x}} + k_z^{(t)} \hat{\mathbf{z}}) \times H_{0y} \hat{\mathbf{y}} = -(\omega/c Z_0) n_b^2(\omega) (E_{0x} \hat{\mathbf{x}} + E_{0z} \hat{\mathbf{z}})$.

replacing ε_0 with $1/(cZ_0)$

Equating the x , y , and z components appearing on the two sides of the above equation, we find

$$i(\omega/c) \sqrt{n_a^2(\omega) \sin^2 \theta - n_b^2(\omega)} H_{0y} = -(\omega/c Z_0) n_b^2(\omega) E_{0x},$$

$$E_{0y} = 0,$$

$$(\omega/c) n_a(\omega) \sin \theta H_{0y} = -(\omega/c Z_0) n_b^2(\omega) E_{0z}^{(t)}.$$

Further simplification now yields

$$E_{0x} = -i Z_0 H_{0y} \sqrt{n_a^2(\omega) \sin^2 \theta - n_b^2(\omega)} / n_b^2(\omega),$$

$$E_{0z} = -Z_0 H_{0y} n_a(\omega) \sin \theta / n_b^2(\omega).$$

Complete expressions for the evanescent \mathbf{E} and \mathbf{H} fields may finally be written down, as follows:

$$\mathbf{E}^{(t)}(\mathbf{r}, t) = (E_{0x} \hat{\mathbf{x}} + E_{0z} \hat{\mathbf{z}}) \exp[i(k_x x + k_z^{(t)} z - \omega t)]$$

$$= -(Z_0 H_{0y} / n_b) [i \sqrt{(n_a \sin \theta / n_b)^2 - 1} \hat{\mathbf{x}} + (n_a \sin \theta / n_b) \hat{\mathbf{z}}]$$

$$\times \exp[(n_b \omega / c) \sqrt{(n_a \sin \theta / n_b)^2 - 1} z] \exp[i(k_x x - \omega t)].$$

$$\mathbf{H}^{(t)}(\mathbf{r}, t) = H_{0y} \hat{\mathbf{y}} \exp[(n_b \omega / c) \sqrt{(n_a \sin \theta / n_b)^2 - 1} z] \exp[i(k_x x - \omega t)].$$

e) In the absence of free charges (i.e., $\rho_{\text{free}} = 0$), Maxwell's 1st equation (within the transmission medium) reduces to $\nabla \cdot \mathbf{D}^{(t)} = \epsilon_0 \epsilon_b(\omega) \nabla \cdot \mathbf{E}^{(t)} = 0$. For the evanescent wave, the satisfaction this equation requires that $\mathbf{k}^{(t)} \cdot \mathbf{E}_0^{(t)}$ vanish. This constraint is readily satisfied, since we have

$$\begin{aligned} \mathbf{k}^{(t)} \cdot \mathbf{E}_0^{(t)} &= k_x E_{0x} + k_z E_{0z} = (n_a \omega / c) \sin \theta \left[-i(Z_0 H_{0y} / n_b) \sqrt{(n_a \sin \theta / n_b)^2 - 1} \right] \\ &\quad + [-i(\omega / c) \sqrt{n_a^2 \sin^2 \theta - n_b^2}] (-Z_0 H_{0y} n_a \sin \theta / n_b^2) = 0. \end{aligned}$$

As for Maxwell's 3rd equation, $\nabla \times \mathbf{E} = -\partial_t \mathbf{B}$, we must show that $\mathbf{k}^{(t)} \times \mathbf{E}_0^{(t)} = \omega \mu_0 \mu(\omega) \mathbf{H}_0^{(t)}$.

$$\begin{aligned} k_z^{(t)} E_{0x} - k_x E_{0z} &= [-i(\omega / c) \sqrt{n_a^2 \sin^2 \theta - n_b^2}] [-i Z_0 H_{0y} \sqrt{n_a^2 \sin^2 \theta - n_b^2} / n_b^2] \\ &\quad - (n_a \omega / c) \sin \theta (-Z_0 H_{0y} n_a \sin \theta / n_b^2) \\ &= -(\omega / c) [(n_a \sin \theta / n_b)^2 - 1] Z_0 H_{0y} + (\omega / c) (n_a \sin \theta / n_b)^2 Z_0 H_{0y} \\ &= (\omega / c) Z_0 H_{0y} = \omega \mu_0 H_{0y}. \end{aligned}$$

$$\begin{aligned} \text{f) } \langle \mathbf{S}(\mathbf{r}, t) \rangle &= \frac{1}{2} \text{Re}(\mathbf{E} \times \mathbf{H}^*) = \frac{1}{2} \text{Re}[(E_{0x} \hat{\mathbf{x}} + E_{0z} \hat{\mathbf{z}}) \times H_{0y}^* \hat{\mathbf{y}}] \exp(2|k_z^{(t)}|z) \\ &= \frac{1}{2} \text{Re}(E_{0x} H_{0y}^* \hat{\mathbf{z}} - E_{0z} H_{0y}^* \hat{\mathbf{x}}) \exp[2(\omega / c) \sqrt{n_a^2 \sin^2 \theta - n_b^2} z] \\ &= Z_0 |H_{0y}|^2 (n_a \sin \theta / 2n_b^2) \exp[(2n_b \omega / c) \sqrt{(n_a \sin \theta / n_b)^2 - 1} z] \hat{\mathbf{x}}. \end{aligned}$$

Note that the z-component of the time-averaged Poynting vector has disappeared from the above equation since $E_{0x} H_{0y}^*$ is purely imaginary. Also, the Poynting vector has no y-component. The energy flow rate does have a component along the x-axis, which rapidly decays as $z \rightarrow -\infty$.

Problem 2) a) From the dispersion relation, the magnitude of the k -vector in free space is found to be $k = \omega/c$. Considering that both \mathbf{k}_1 and \mathbf{k}_2 are in the xz -plane (i.e., $k_y = 0$), we will have

$$\mathbf{k}_1 = (\omega/c)(\cos \theta \hat{\mathbf{x}} + \sin \theta \hat{\mathbf{z}}). \quad (1)$$

$$\mathbf{E}_1(\mathbf{r}, t) = \mathbf{E}_{o1} \exp[i(\mathbf{k}_1 \cdot \mathbf{r} - \omega t)] = E_0 \hat{\mathbf{y}} \exp[i(\omega/c)(x \cos \theta + z \sin \theta - ct)]. \quad (2)$$

$$\begin{aligned} \mathbf{H}_1(\mathbf{r}, t) &= \mathbf{H}_{o1} \exp[i(\mathbf{k}_1 \cdot \mathbf{r} - \omega t)] \\ &= (E_0/Z_0)(-\sin \theta \hat{\mathbf{x}} + \cos \theta \hat{\mathbf{z}}) \exp[i(\omega/c)(x \cos \theta + z \sin \theta - ct)]. \end{aligned} \quad (3)$$

Similarly,

$$\mathbf{k}_2 = (\omega/c)(\cos \theta \hat{\mathbf{x}} - \sin \theta \hat{\mathbf{z}}). \quad (4)$$

$$\mathbf{E}_2(\mathbf{r}, t) = \mathbf{E}_{o2} \exp[i(\mathbf{k}_2 \cdot \mathbf{r} - \omega t)] = E_0 \hat{\mathbf{y}} \exp[i(\omega/c)(x \cos \theta - z \sin \theta - ct)]. \quad (5)$$

$$\begin{aligned} \mathbf{H}_2(\mathbf{r}, t) &= \mathbf{H}_{o2} \exp[i(\mathbf{k}_2 \cdot \mathbf{r} - \omega t)] \\ &= (E_0/Z_0)(\sin \theta \hat{\mathbf{x}} + \cos \theta \hat{\mathbf{z}}) \exp[i(\omega/c)(x \cos \theta - z \sin \theta - ct)]. \end{aligned} \quad (6)$$

b) Considering that $H_y = 0$ and that H_x and H_z do not depend on the y -coordinate, the expression of the curl of \mathbf{H} (evaluated in the plane of the sheet at $z = 0$) is simplified, as follows:

$$\nabla \times \mathbf{H} = \underbrace{(\partial_z H_x - \partial_x H_z)}_{\substack{\text{ordinary differentiation of } H_z \text{ with respect to } x, \text{ since } H_z \text{ is continuous at } z = 0 \\ \partial_z H_x \cong \Delta H_x / \Delta z = [H_x(x, z = d/2, t) - H_x(x, z = -d/2, t)]/d}} \hat{\mathbf{y}} \cong \left(-\frac{2E_0 \sin \theta}{Z_0 d} - \frac{iE_0 \omega \cos^2 \theta}{Z_0 c} \right) \hat{\mathbf{y}} e^{i(\omega/c)(x \cos \theta - ct)}. \quad (7)$$

Since $\mathbf{D}(\mathbf{r}, t) = \varepsilon_0 \mathbf{E} + \mathbf{P} = \varepsilon_0 E_0 \hat{\mathbf{y}} e^{i(\omega/c)(x \cos \theta - ct)} + P_0 \hat{\mathbf{y}} e^{i(\kappa_0 x - \omega t - \varphi_0)}$, equating $\nabla \times \mathbf{H}$ of Eq.(7) with $\partial_t \mathbf{D} = -i\omega \mathbf{D}(\mathbf{r}, t)$ reveals that $\kappa_0 = (\omega/c) \cos \theta$.

c) Continuity of \mathbf{E}_\parallel is satisfied, as the E -field on both sides of the sheet is $E_0 \hat{\mathbf{y}} e^{i(\omega/c)(x \cos \theta - ct)}$. This is also the E -field inside the sheet, acting on the electric dipoles of the material.

Similarly, the continuity of \mathbf{B}_\perp is automatically satisfied, as the perpendicular B -field on both sides of the sheet is seen from Eqs.(3) and (6) to be $\mu_0 H_z = (E_0/c) \cos \theta e^{i(\omega/c)(x \cos \theta - ct)}$.

The tangential H -field (i.e., H_x) is discontinuous at the surface of the sheet, being equal to $\pm(E_0/Z_0) \sin \theta e^{i(\omega/c)(x \cos \theta - ct)}$ on the left- and right-hand sides, respectively; see Eqs.(3) and (6). Inside the dielectric material, the D -field is $\mathbf{D}(\mathbf{r}, t) = (\varepsilon_0 E_0 + P_0 e^{-i\varphi_0}) \hat{\mathbf{y}} e^{i(\omega/c)(x \cos \theta - ct)}$. Considering that, in the absence of free currents (i.e., $\mathbf{J}_{\text{free}} = 0$), $\nabla \times \mathbf{H} = \partial_t \mathbf{D} = -i\omega \mathbf{D}$, and that the sheet thickness d is sufficiently small, we arrive at

$$\frac{2E_0 \sin \theta}{Z_0 d} \cong i\omega(\varepsilon_0 E_0 + P_0 e^{-i\varphi_0}). \quad (8)$$

The approximate equality in the above equation becomes exact in the limit when $d \rightarrow 0$. The near equality in Eq.(8) could also be obtained with the aid of Eq.(7), where the first term on the right-hand side of Eq.(7) dominates the second term when $d \ll c/\omega = \lambda_0/2\pi$.

d) For the incident beam at the location of the sheet (i.e., at $z = 0$), we have

$$\nabla \times \mathbf{H}^{(\text{inc})} = \partial_t \mathbf{D}^{(\text{inc})} = -i\omega \varepsilon_0 \mathbf{E}^{(\text{inc})} = -\left(\frac{iE_0^{(\text{inc})} \omega}{Z_0 c} \right) \hat{\mathbf{y}} e^{i(\omega/c)(x \cos \theta - ct)}. \quad (9)$$

The above contribution to the curl of the H -field at $z = 0$ should now be added to Eq.(7). However, for $d \ll c/\omega = \lambda_0/2\pi$, we may ignore this contribution of the incident beam, just as we ignored the second term on the right-hand side of Eq.(7). Consequently, for a sufficiently thin sheet, $\nabla \times \mathbf{H}$ will be dominated by the discontinuity in \mathbf{H}_{\parallel} across the sheet produced by the two radiated plane-waves. Given that $\mathbf{D}(\mathbf{r}, t) = \varepsilon_0 \varepsilon(\omega)(E_0^{(\text{inc})} + E_0)\hat{\mathbf{y}}e^{i(\omega/c)(x \cos \theta - ct)}$, application of Maxwell's 2nd equation, $\nabla \times \mathbf{H} = \partial_t \mathbf{D} = -i\omega \mathbf{D}$, now yields

$$(2E_0 \sin \theta / Z_0 d) e^{i(\omega/c)(x \cos \theta - ct)} \cong i\omega \varepsilon_0 \varepsilon(\omega)(E_0^{(\text{inc})} + E_0) e^{i(\omega/c)(x \cos \theta - ct)}. \quad (10)$$

Solving the above equation for the reflected field amplitude E_0 , we find

$$E_0 \cong -\frac{E_0^{(\text{inc})}}{1 + i[2c \sin \theta / \omega \varepsilon(\omega) d]} \rightarrow E_0 / E_0^{(\text{inc})} \cong -\frac{\pi \varepsilon(\omega) d}{\pi \varepsilon(\omega) d + i\lambda_0 \sin \theta}. \quad \leftarrow \boxed{\lambda_0 = 2\pi c / \omega} \quad (11)$$

e) The transmitted E -field is readily found from Eq.(10), as follows:

$$E_0^{(\text{trans})} = E_0^{(\text{inc})} + E_0 \cong \frac{(2E_0 / Z_0 d) \sin \theta}{i\omega \varepsilon_0 \varepsilon(\omega)} \rightarrow E_0^{(\text{trans})} / E_0^{(\text{inc})} \cong \frac{i\lambda_0 \sin \theta}{\pi \varepsilon(\omega) d + i\lambda_0 \sin \theta}. \quad (12)$$

Digression. Setting $\theta = 45^\circ$, and $\varepsilon(\omega) = \lambda_0 / (\sqrt{2}\pi d)$, the reflection coefficient obtained from Eq.(11) will be

$$E_0 / E_0^{(\text{inc})} = -1 / (1 + i) = e^{i3\pi/4} / \sqrt{2}. \quad (13)$$

Similarly, Eq.(12) yields the transmission coefficient, as follows:

$$E_0^{(\text{trans})} / E_0^{(\text{inc})} = i / (1 + i) = e^{i\pi/4} / \sqrt{2}. \quad (14)$$

Both the reflected and transmitted E -field amplitudes are seen to be $1/\sqrt{2}$ times that of the incident E -field. While the reflected E -field is phase-shifted (relative to the incident E -field) by 135° , the relative phase-shift of the transmitted E -field is 45° . The thin dielectric sheet thus exhibits the essential characteristics of a 50/50 beam-splitter. Note that, for this to hold to a good approximation, the required value of $\varepsilon(\omega)$, namely, $\lambda_0 / (\sqrt{2}\pi d)$, may have to be impractically large, given that d needs to be substantially smaller than the incident wavelength. In fact, recalling that $n(\omega) = \sqrt{\varepsilon(\omega)}$, the relation between d and the wavelength λ_0/n inside the dielectric medium will be $\lambda_0 / nd = \sqrt{2}\pi n$. For d to be only one-tenth of λ_0/n , it will be necessary to have $n = 2.25$.
